



Fig. 1. Beryllium pressure vessel, sectional view, including cap and piston. Beryllium cylinder is stippled. Inset shows view of vessel and cap, and relations between casing slots and beryllium cylinder.

exterior band of copper or brass sheeting (see Fig. 2). A special cooling jacket was constructed to fit around the ram and goniometer spindle.

The temperature was measured by means of a Chromel-alumel thermocouple insulated and inserted into hole F of plug B, Fig. 1. The temperature was read from a Leeds-Northrup potentiometer (with a "reference junction" to approximate the cold-junction correction). Insertion of a mercury thermometer into the bomb window at 175°C gave results within two degrees of that read from the potentiometer. Work with the transition point of $\text{KNO}_3\text{-II-KNO}_3\text{-I}$ (128.3°C) showed that thermocouple readings were correct to within ± 2 deg. A similar uncertainty can be assigned to the results of this investigation. Excessive heat flow out through the vessel was eliminated by placing a 4-mm disk of Transite between the piston base and plug base (B, Fig. 1).

Preliminary experiments were carried out to determine the difference between nominal and internal pressures. This was done by making a standard run using a highly compressible material, such as KI or RbI, as a sample. Previously determined equations giving $\Delta v/v_0$ as a function of pressure allow calculation of internal pressures from peak shift on the diffraction chart. To correct for the peak shift due to change in sample height (mainly due to compression of Transite pad and beryllium pellet above the sample) a thin layer of diamond powder was placed on top of the sample pellet. Effective reflecting

depths of diamond powder and sample material would be almost identical after a slight amount of pressure was applied to imbed the diamond into the sample.

The calibration runs carried out specifically for this study agreed closely with results obtained previously with the same vessels. Using a piston that fits easily into the cylinder, there is very little frictional loss of pressure on going up in pressure. After perhaps 20 kb had been attained the return run indicated considerable lag of the internal pressure above nominal pressure. At $P = 0$ (nominal) on the return run, the internal pressure may be as much as 4 kb. One up-pressure run at 150°C indicated that there is less frictional resistance than at room temperature, after taking into account the change in compressibility of sample with temperature. There is still some pressure uncertainty stemming from the deformation of the beryllium pellet and vessel walls, especially at higher temperatures. This deformation is most likely responsible for the pressure lag on the return leg of the runs as well as increased frictional resistance when repeating a run with the same sample and beryllium pellet used previously. A pressure uncertainty of ± 1 kb is appended to all pressure values, and at temperatures below 100°C this figure is considered to be quite conservative.

Radiation used was $\text{MoK}\alpha$, with applied power of 40 kV and 20 mA. A scintillation counter combined with pulse-height analyser comprised the detection,

AMS

licating a critical end point for although Pontiatovskii stated point where the heat of transition was not necessarily the end point.

work by HERMANN and SWENSON and SWENSON⁽²³⁾ confirms transition volumes decrease with pressure and pressure along the line and Swenson extrapolate to 20,000 atm as the point of volume change. Of importance will be the fact that Beecroft observed a spreading out of the transition at higher temperatures and a change in thermal expansion of phase II) at 20,000 atm, over pressure. The earlier work of SWENSON⁽²²⁾ revealed the transition at room temperature work, using the cerium revealed little or no hys-

EXPERIMENTAL METHOD

to that previously described. A sketch of the supported vessel is given in Fig. 1. The vessel is less than 6 cm high and is mounted at the base of a small press. The spindle is inserted into the goniometer as seen in the arrangement, Fig. 2.

The vessel is encased in a steel jacket into the hardened steel outer casing there is a selection of removable caps and corresponding piston and different sample sizes and the pump system now in use. The vessel used throughout the study is a 25 mm. beryllium pellet to be used for X-rays. The X-ray beam is directed through the outer casing (Fig. 1, inset), around the pellet, and onto the detector which is similar. The dial gauge is used to measure the main function of the vessel, the main function of the vessel, the main function of the vessel.

The heating jacket made from Nichrome V wire wound around the vessel is fashioned into a zig-zag belt. It consists of an inner and outer layer of insulation, or by layers of Transite and diamond powder held together by an